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Pd_{2.28(1)}Zn_{10.37(1)}Al_{0.35(1)}, a ternary *y*-brass-type structure

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Key indicators: single-crystal X-ray study; T = 293 K; mean σ () = 0.002 Å; disorder in main residue; R factor = 0.027; wR factor = 0.068; data-to-parameter ratio = 15.4.

Palladium zinc aluminium (2.28/10.37/0.35), $Pd_{2.28(1)}Zn_{10.37(1)}$ -Al_{0.35(1)}, represents the upper limit of Al substitution into the parent cubic γ -brass $Pd_{2+x}Zn_{11-x}$. The structure can be described in terms of a 26-atom cluster consisting of an inner tetrahedron (IT), an outer tetrahedron (OT), an octahedron (OH) and a cuboctahedron (CO), with the substituted Al atoms partially occupying the IT (.3*m*) and CO (..*m*) sites.

Related literature

For related literature, see: Arnberg & Westman (1972); Edström & Westman (1969); Gross *et al.* (2001); Gourdon & Miller (2006); Harbrecht *et al.* (2002); Thimmaiah & Miller (2010). For standardization of crystal structures, see: Gelato & Parthé (1987).

Experimental

Crystal data

 $Pd_{2.28}Zn_{10.37}Al_{0.35}$ $M_r = 929.56$ Cubic, $I\overline{4}3m$ a = 9.1079 (11) Å V = 755.54 (16) Å³ Z = 4Mo Kα radiation $\mu = 37.46 \text{ mm}^{-1}$ T = 293 K0.12 × 0.06 × 0.03 mm

Data collection

Stoe IPDS-II diffractometer Absorption correction: numerical (X-SHAPE and X-RED; Stoe & Cie, 2005) $T_{min} = 0.054, T_{max} = 0.465$

Refinement

 $R[F^2 > 2\sigma(F^2)] = 0.027$ $wR(F^2) = 0.068$ S = 1.02339 reflections 22 parameters 11243 measured reflections 339 independent reflections 337 reflections with $I > 2\sigma(I)$ $R_{int} = 0.069$

 $\begin{array}{l} \Delta \rho_{\rm max} = 1.05 \ {\rm e} \ {\rm \AA}^{-3} \\ \Delta \rho_{\rm min} = -1.19 \ {\rm e} \ {\rm \AA}^{-3} \\ {\rm Absolute \ structure: \ Flack \ (1983)} \\ {\rm Flack \ parameter: \ 0.04 \ (4)} \end{array}$

Data collection: X-AREA (Stoe & Cie, 2009); cell refinement: X-AREA; data reduction: X-AREA; program(s) used to solve structure: SHELXS97 (Sheldrick, 2008); program(s) used to refine structure: SHELXL97 (Sheldrick, 2008); molecular graphics: DIAMOND (Brandenburg, 2009); software used to prepare material for publication: SHELXTL (Sheldrick, 2008).

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Supplementary data and figures for this paper are available from the IUCr electronic archives (Reference: MG2090).

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supplementary materials

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Pd_{2.28(1)}Zn_{10.37(1)}Al_{0.35(1)}, a ternary *?*-brass-type structure

S. Thimmaiah and G. J. Miller

Comment

Various M_2 Zn₁₁ phases [M = Rh (Gross *et al.*, 2001), Pd (Gourdon & Miller, 2006), Ir (Arnberg & Westman, 1972), Pt (Harbrecht *et al.*, 2002)] adopt the γ -brass type structure (Pearson code *cI*52). To study the influence of valence electron concentration (vec) on γ -brass type phases, we attempted replacing Zn by Al in the parent Pd_{2 + x}Zn_{11 - x} phase (Gourdon & Miller, 2006). Initially obtained as a side product, Pd_{2.28 (1)}Zn_{10.37 (1)}Al_{0.35 (1)} represents the upper limit of Al substitution in the Pd_{2 + x}Zn_{11 - x} phase. Further substitution of Al leads to 2×2×2 superstructures of γ -brass with lattice parameters ranging from 18.0700 (3) to 18.1600 (2) Å (Pearson code *cF*400–*cF*416) (Thimmaiah & Miller, 2010).

In terms of the 26-atom clusters (in *bcc* arrangement) commonly used to describe the structure of γ -brass, the inner tetrahedron (IT) and cuboctahedron (CO) are occupied by mixtures of Zn and Al atoms, the outer tetrahedron (OT) is fully occupied by Pd atoms, and the octahedron (OH) is occupied by a mixture of Zn and Pd atoms (Fig. 1a). Similar mixing of Zn and Pd atoms on the OH sites is observed in binary Pd_{2 + x}Zn_{11 - x} (Gourdon & Miller, 2006; Edström & Westman, 1969). An alternative description involves four interpenetrating icosahedra, which are constructed around each OT atom and encapsulate a tetrahedron formed by IT atoms (Fig. 1 b). The IT and OT sites are each surrounded by 12 nearest neighbours [at distances of 2.666 (1)–2.789 (2) Å and 2.624 (1)–2.794 (1) Å, respectively] forming distorted icosahedra. On the other hand, the coordination numbers are 13 around the OH site [2.591 (2)–2.945 (1) Å] and 11 around the CO site [2.612 (1)–2.945 (1) Å].

Experimental

The title compound was prepared from 0.5 - g mixtures of the elements (Pd foil, MPC, Ames Laboratory, 99.999%; Zn ingot, MPC, Ames Laboratory, 99.999%; Al tear drop, MPC, Ames Laboratory, 99.999%) loaded into cleaned Ta tubes, which were placed in evacuated (10^{-5} torr) and sealed silica tubes. The tubes were heated at 30 °C h⁻¹ to 850 °C, kept there for 12 h, cooled to 550 °C over 12 h, equilibrated there for 3 d, and then cooled to room temperature by shutting off the furnace.

Refinement

Refinement of a starting model (Gourdon & Miller, 2006) led to a mixture of 0.09 (3) Pd and 0.91 (3) Zn in the OH sites. However, the IT and CO sites, initially assumed to be fully occupied by Zn atoms, exhibited elevated isotropic displacement parameters. Modeling these sites with a mixture of Zn and Al resulted in the refined composition $Pd_{2.28 (1)}Zn_{10.37 (1)}Al_{0.35 (1)}$. Analysis of multiple crystals obtained from the same and other batches gave the same site occupancies. Within the limitation of the technique, semiquantitative energy-dispersive X-ray analysis corroborate this chemical composition. The structure was standardized by means of the program *STRUCTURE TIDY* (Gelato & Parthé, 1987). The highest peak and the deepest hole are located 1.26 Å and 1.18 Å, respectively, from Pd1.

Figures



Fig. 1. Cubic γ -brass structure of Pd_{2.28 (1)}Zn_{10.37 (1)}Al_{0.35 (1)} in terms of (*a*) 26-atom clusters in *bcc* arrangement, with different polyhedra emphasized, and (*b*) four interpenetrating Pd-centered icosahedra. The color scheme is shown and displacement ellipsoids are drawn at the 90% probability level.

Melting point: not measured K

Mo *K* α radiation, $\lambda = 0.71073$ Å

 $\theta = 3.2 - 34.8^{\circ}$

 $\mu = 37.46 \text{ mm}^{-1}$ T = 293 K

Rectangular, silver

 $0.12 \times 0.06 \times 0.03 \text{ mm}$

Cell parameters from 2000 reflections

palladium zinc aluminium (2.28/10.37/0.35)

Crystal data

Pd_{2.28}Zn_{10.37}Al_{0.35} $M_r = 929.56$ Cubic, $I\overline{4}3m$ Hall symbol: I -4 2 3 a = 9.1079 (11) Å V = 755.54 (16) Å³ Z = 4 F(000) = 1681 $D_x = 8.172$ Mg m⁻³

Data collection

| Stoe/IPDS-II diffractometer | 339 independent reflections |
|--|---|
| Radiation source: fine-focus sealed tube | 337 reflections with $I > 2\sigma(I)$ |
| graphite | $R_{\rm int} = 0.069$ |
| ϕ and ω scans | $\theta_{\text{max}} = 34.8^{\circ}, \ \theta_{\text{min}} = 3.2^{\circ}$ |
| Absorption correction: numerical (<i>X-SHAPE</i> and <i>X-RED</i> ; Stoe & Cie, 2005) | $h = -14 \rightarrow 14$ |
| $T_{\min} = 0.054, T_{\max} = 0.465$ | $k = -14 \rightarrow 13$ |
| 11243 measured reflections | $l = -14 \rightarrow 14$ |

Refinement

| Refinement on F^2 | Secondary atom site location: difference Fourier map |
|---------------------------------|--|
| Least-squares matrix: full | $w = 1/[\sigma^2(F_o^2) + (0.0249P)^2 + 32.9721P]$ where $P = (F_o^2 + 2F_c^2)/3$ |
| $R[F^2 > 2\sigma(F^2)] = 0.027$ | $(\Delta/\sigma)_{\rm max} < 0.001$ |
| $wR(F^2) = 0.068$ | $\Delta \rho_{max} = 1.05 \text{ e } \text{\AA}^{-3}$ |
| <i>S</i> = 1.02 | $\Delta \rho_{\rm min} = -1.19 \text{ e } \text{\AA}^{-3}$ |
| 339 reflections | Extinction correction: <i>SHELXL97</i> (Sheldrick, 2008), Fc [*] =kFc[1+0.001xFc ² λ^3 /sin(2 θ)] ^{-1/4} |
| 22 parameters | Extinction coefficient: 0.00118 (16) |
| 0 restraints | Absolute structure: Flack (1983) |

Primary atom site location: structure-invariant direct Flack parameter: 0.04 (4)

Special details

Geometry. All e.s.d.'s (except the e.s.d. in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell e.s.d.'s are taken into account individually in the estimation of e.s.d.'s in distances, angles and torsion angles; correlations between e.s.d.'s in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell e.s.d.'s is used for estimating e.s.d.'s involving l.s. planes.

Refinement. Refinement of F^2 against ALL reflections. The weighted *R*-factor *wR* and goodness of fit *S* are based on F^2 , conventional *R*-factors *R* are based on *F*, with *F* set to zero for negative F^2 . The threshold expression of $F^2 > \sigma(F^2)$ is used only for calculating *R*-factors(gt) *etc*. and is not relevant to the choice of reflections for refinement. *R*-factors based on F^2 are statistically about twice as large as those based on *F*, and *R*- factors based on ALL data will be even larger.

| | x | У | Z | | $U_{\rm iso}*/U_{\rm eq}$ | Occ. (<1) |
|------------------------|-------------------|-------------|-----------------|-----------------------|---------------------------|-------------|
| Pd1 | 0.32674 (6) | 0.32674 (| 6) 0.3 | 2674 (6) | 0.0101 (3) | |
| Zn1 | 0.10828 (12) | 0.10828 (| 12) 0.1 | 0828 (12) | 0.0139 (5) | 0.924 (17) |
| Al1 | 0.10828 (12) | 0.10828 (| 12) 0.1 | 0828 (12) | 0.0139 (5) | 0.076 (17) |
| Zn2 | 0.35776 (15) | 0.0000 | 0.0 | 0000 | 0.0135 (5) | 0.91 (3) |
| Pd2 | 0.35776 (15) | 0.0000 | 0.0 | 0000 | 0.0135 (5) | 0.09 (3) |
| Zn3 | 0.31076 (9) | 0.31076 (| 9) 0.0 | 3932 (12) | 0.0162 (3) | 0.966 (13) |
| A13 | 0.31076 (9) | 0.31076 (| 9) 0.0 | 3932 (12) | 0.0162 (3) | 0.034 (13) |
| Atomic displac | cement parameters | $(Å^2)$ | | | | |
| | U^{11} | U^{22} | U ³³ | U^{12} | U^{13} | U^{23} |
| Pd1 | 0.0101 (3) | 0.0101 (3) | 0.0101 (3) | 0.0007 (2) | 0.0007 (2) | 0.0007 (2) |
| Zn1 | 0.0139 (5) | 0.0139 (5) | 0.0139 (5) | 0.0029 (4) | 0.0029 (4) | 0.0029 (4) |
| Al1 | 0.0139 (5) | 0.0139 (5) | 0.0139 (5) | 0.0029 (4) | 0.0029 (4) | 0.0029 (4) |
| Zn2 | 0.0124 (7) | 0.0140 (6) | 0.0140 (6) | 0.000 | 0.000 | 0.0034 (5) |
| Pd2 | 0.0124 (7) | 0.0140 (6) | 0.0140 (6) | 0.000 | 0.000 | 0.0034 (5) |
| Zn3 | 0.0177 (4) | 0.0177 (4) | 0.0132 (5) | -0.0026 (3) | -0.0028 (2) | -0.0028 (2) |
| A13 | 0.0177 (4) | 0.0177 (4) | 0.0132 (5) | -0.0026 (3) | -0.0028 (2) | -0.0028 (2) |
| Geometric par | rameters (Å, °) | | | | | |
| Pd1—Al3 ⁱ | | 2.6240 (11) | Zn | 1—Zn3 | 2. | .6826 (17) |
| Pd1—Zn3 ⁱ | | 2.6240 (11) | Zn | 2—Pd2 ^{vi} | 2. | .591 (3) |
| Pd1—Al3 ⁱⁱ | | 2.6240 (11) | Zn | 2—Zn2 ^{vi} | 2. | .591 (3) |
| Pd1—Al3 ⁱⁱⁱ | | 2.6240 (11) | Zn | 2—A13 ^{vii} | 2. | .6115 (12) |
| Pd1—Zn3 ⁱⁱ | | 2.6240 (11) | Zn | 2—Zn3 ^{vii} | 2. | .6115 (12) |
| Pd1—Zn3 ⁱⁱⁱ | | 2.6240 (11) | Zn | 2—Al3 ^{viii} | 2. | .6115 (12) |
| Pd1—Al3 ^{iv} | | 2.6259 (12) | Zn | 2—Zn3 ^{viii} | 2. | .6115 (12) |
| Pd1—Zn3 ^{iv} | | 2.6259 (12) | Zn | 2—Zn1 ^{ix} | 2. | .6662 (12) |
| | | | | | | |

Fractional atomic coordinates and isotropic or equivalent isotropic displacement parameters (A^2)

| Pd1—Al3 ^v | 2.6259 (12) | Zn2—Al1 ^{ix} | 2.6662 (12) |
|--|--------------|--|-------------|
| Pd1—Zn3 ^v | 2.6259 (12) | Zn2—Pd1 ^x | 2.7936 (9) |
| Pd1—Zn3 | 2.6259 (12) | Zn2—Pd1 ^{xi} | 2.7936 (9) |
| Zn1—Zn2 | 2.6662 (12) | Zn3—Pd2 ⁱ | 2.6115 (12) |
| Zn1—Pd2 ^v | 2.6662 (12) | Zn3—Zn2 ⁱ | 2.6115 (12) |
| Zn1—Pd2 ^{iv} | 2.6662 (12) | Zn3—Pd1 ^x | 2.6240 (11) |
| Zn1—Zn2 ^v | 2.6662 (12) | Zn3—Al3 ^{xii} | 2.7245 (6) |
| Zn1—Zn2 ^{iv} | 2.6662 (12) | Zn3—Al3 ^{vii} | 2.7245 (6) |
| Zn1—Al3 ^v | 2.6826 (17) | Zn3—Zn3 ^{xii} | 2.7245 (6) |
| Zn1—Al3 ^{iv} | 2.6826 (17) | Zn3—Zn3 ^{vii} | 2.7245 (6) |
| Zn1—Zn3 ^v | 2.6826 (17) | Zn3—Al3 ⁱ | 2.7245 (6) |
| Zn1—Zn3 ^{iv} | 2.6826 (17) | Zn3—Al3 ⁱⁱ | 2.7245 (6) |
| Al3 ⁱ —Pd1—Zn3 ⁱ | 0.00 (6) | Al3 ^{vii} —Zn2—Zn3 ^{vii} | 0.00 (5) |
| Al3 ⁱ —Pd1—Al3 ⁱⁱ | 118.459 (14) | Pd2 ^{vi} —Zn2—Al3 ^{viii} | 68.97 (4) |
| Zn3 ⁱ —Pd1—Al3 ⁱⁱ | 118.459 (14) | Zn2 ^{vi} —Zn2—Al3 ^{viii} | 68.97 (4) |
| Al3 ⁱ —Pd1—Al3 ⁱⁱⁱ | 118.459 (14) | Al3 ^{vii} —Zn2—Al3 ^{viii} | 137.93 (7) |
| Zn3 ⁱ —Pd1—Al3 ⁱⁱⁱ | 118.459 (14) | Zn3 ^{vii} —Zn2—Al3 ^{viii} | 137.93 (7) |
| Al3 ⁱⁱ —Pd1—Al3 ⁱⁱⁱ | 118.459 (14) | Pd2 ^{vi} —Zn2—Zn3 ^{viii} | 68.97 (4) |
| Al3 ⁱ —Pd1—Zn3 ⁱⁱ | 118.459 (14) | Zn2 ^{vi} —Zn2—Zn3 ^{viii} | 68.97 (4) |
| Zn3 ⁱ —Pd1—Zn3 ⁱⁱ | 118.459 (14) | Al3 ^{vii} —Zn2—Zn3 ^{viii} | 137.93 (7) |
| Al3 ⁱⁱ —Pd1—Zn3 ⁱⁱ | 0.00 (6) | Zn3 ^{vii} —Zn2—Zn3 ^{viii} | 137.93 (7) |
| A13 ⁱⁱⁱ —Pd1—Zn3 ⁱⁱ | 118.459 (14) | Al3 ^{viii} —Zn2—Zn3 ^{viii} | 0.00 (3) |
| Al3 ⁱ —Pd1—Zn3 ⁱⁱⁱ | 118.459 (14) | Pd2 ^{vi} —Zn2—Zn1 | 148.46 (4) |
| Zn3 ⁱ —Pd1—Zn3 ⁱⁱⁱ | 118.459 (14) | Zn2 ^{vi} —Zn2—Zn1 | 148.46 (4) |
| Al3 ⁱⁱ —Pd1—Zn3 ⁱⁱⁱ | 118.459 (14) | Al3 ^{vii} —Zn2—Zn1 | 107.81 (3) |
| Al3 ⁱⁱⁱ —Pd1—Zn3 ⁱⁱⁱ | 0.00 (6) | Zn3 ^{vii} —Zn2—Zn1 | 107.81 (3) |
| Zn3 ⁱⁱ —Pd1—Zn3 ⁱⁱⁱ | 118.459 (14) | Al3 ^{viii} —Zn2—Zn1 | 107.81 (3) |
| Al3 ⁱ —Pd1—Al3 ^{iv} | 62.53 (3) | Zn3 ^{viii} —Zn2—Zn1 | 107.81 (3) |
| Zn3 ⁱ —Pd1—Al3 ^{iv} | 62.53 (3) | Pd2 ^{vi} —Zn2—Zn1 ^{ix} | 148.46 (4) |
| Al3 ⁱⁱ —Pd1—Al3 ^{iv} | 133.05 (4) | Zn2 ^{vi} —Zn2—Zn1 ^{ix} | 148.46 (4) |
| Al3 ⁱⁱⁱ —Pd1—Al3 ^{iv} | 62.53 (3) | Al3 ^{vii} —Zn2—Zn1 ^{ix} | 107.81 (3) |
| Zn3 ⁱⁱ —Pd1—Al3 ^{iv} | 133.05 (4) | Zn3 ^{vii} —Zn2—Zn1 ^{ix} | 107.81 (3) |
| Zn3 ⁱⁱⁱ —Pd1—Al3 ^{iv} | 62.53 (3) | Al3 ^{viii} —Zn2—Zn1 ^{ix} | 107.81 (3) |
| Al3 ⁱ —Pd1—Zn3 ^{iv} | 62.53 (3) | Zn3 ^{viii} —Zn2—Zn1 ^{ix} | 107.81 (3) |
| Zn3 ⁱ —Pd1—Zn3 ^{iv} | 62.53 (3) | Zn1—Zn2—Zn1 ^{ix} | 63.08 (9) |
| Al3 ⁱⁱ —Pd1—Zn3 ^{iv} | 133.05 (4) | Pd2 ^{vi} —Zn2—Al1 ^{ix} | 148.46 (4) |
| Al3 ⁱⁱⁱ —Pd1—Zn3 ^{iv} | 62.53 (3) | Zn2 ^{vi} —Zn2—A11 ^{ix} | 148.46 (4) |
| Zn3 ⁱⁱ —Pd1—Zn3 ^{iv} | 133.05 (4) | Al3 ^{vii} —Zn2—Al1 ^{ix} | 107.81 (3) |
| Zn3 ⁱⁱⁱ —Pd1—Zn3 ^{iv} | 62.53 (3) | Zn3 ^{vii} —Zn2—Al1 ^{ix} | 107.81 (3) |
| | | | |

| i v | | VIII 1V | |
|--|--------------|--|------------|
| Al3 ¹ —Pd1—Al3 ^v | 133.05 (4) | $Zn3^{vm}$ — $Zn2$ — $Al1^{lx}$ | 107.81 (3) |
| $Zn3^{1}$ —Pd1—Al3 ^v | 133.05 (4) | Zn1—Zn2—All ^{1x} | 63.08 (9) |
| $A13^{II}$ $Pd1$ $A13^{V}$ | 62.53 (3) | $Zn1^{1x}$ — $Zn2$ — $A11^{1x}$ | 0.00 (6) |
| $A13^{11}$ $Pd1$ $A13^{v}$ | 62.53 (3) | $Pd2^{v_1}$ —Zn2—Pd1 ^x | 126.98 (3) |
| $Zn3^{n}$ —Pd1—Al3 ^v | 62.53 (3) | $Zn2^{v_1}$ — $Zn2$ — $Pd1^x$ | 126.98 (3) |
| Zn3 ⁱⁱⁱ —Pd1—Al3 ^v | 62.53 (3) | $A13^{vii}$ —Zn2—Pd1 ^x | 58.01 (3) |
| $A13^{iv}$ —Pd1—A13 ^v | 83.48 (4) | $Zn3^{vii}$ — $Zn2$ — $Pd1^{x}$ | 58.01 (3) |
| Zn3 ^{iv} —Pd1—Al3 ^v | 83.48 (4) | Al3 ^{viii} —Zn2—Pd1 ^x | 164.05 (6) |
| Al3 ⁱ —Pd1—Zn3 ^v | 133.05 (4) | Zn3 ^{viii} —Zn2—Pd1 ^x | 164.05 (6) |
| Zn3 ⁱ —Pd1—Zn3 ^v | 133.05 (4) | Zn1—Zn2—Pd1 ^x | 59.16 (3) |
| Al3 ⁱⁱ —Pd1—Zn3 ^v | 62.53 (3) | $Zn1^{ix}$ — $Zn2$ — $Pd1^{x}$ | 59.16 (3) |
| Al3 ⁱⁱⁱ —Pd1—Zn3 ^v | 62.53 (3) | All ^{ix} —Zn2—Pd1 ^x | 59.16 (3) |
| Zn3 ⁱⁱ —Pd1—Zn3 ^v | 62.53 (3) | Pd2 ^{vi} —Zn2—Pd1 ^{xi} | 126.98 (3) |
| Zn3 ⁱⁱⁱ —Pd1—Zn3 ^v | 62.53 (3) | Zn2 ^{vi} —Zn2—Pd1 ^{xi} | 126.98 (3) |
| Al3 ^{iv} —Pd1—Zn3 ^v | 83.48 (4) | Al3 ^{vii} —Zn2—Pd1 ^{xi} | 164.05 (6) |
| Zn3 ^{iv} —Pd1—Zn3 ^v | 83.48 (4) | Zn3 ^{vii} —Zn2—Pd1 ^{xi} | 164.05 (6) |
| Al3 ^v —Pd1—Zn3 ^v | 0.00 (7) | Al3 ^{viii} —Zn2—Pd1 ^{xi} | 58.01 (3) |
| Al3 ⁱ —Pd1—Zn3 | 62.53 (3) | Zn3 ^{viii} —Zn2—Pd1 ^{xi} | 58.01 (3) |
| Zn3 ⁱ —Pd1—Zn3 | 62.53 (3) | Zn1—Zn2—Pd1 ^{xi} | 59.16 (3) |
| Al3 ⁱⁱ —Pd1—Zn3 | 62.53 (3) | Zn1 ^{ix} —Zn2—Pd1 ^{xi} | 59.16 (3) |
| A13 ⁱⁱⁱ —Pd1—Zn3 | 133.05 (4) | All ^{ix} —Zn2—Pd1 ^{xi} | 59.16 (3) |
| Zn3 ⁱⁱ —Pd1—Zn3 | 62.53 (3) | Pd1 ^x —Zn2—Pd1 ^{xi} | 106.04 (6) |
| Zn3 ⁱⁱⁱ —Pd1—Zn3 | 133.05 (4) | Pd2 ⁱ —Zn3—Zn2 ⁱ | 0.00 (5) |
| A13 ^{iv} —Pd1—Zn3 | 83.48 (4) | Pd2 ⁱ —Zn3—Pd1 ^x | 153.49 (6) |
| Zn3 ^{iv} —Pd1—Zn3 | 83.48 (4) | Zn2 ⁱ —Zn3—Pd1 ^x | 153.49 (6) |
| Al3 ^v —Pd1—Zn3 | 83.48 (4) | Pd2 ⁱ —Zn3—Pd1 | 64.47 (4) |
| Zn3 ^v —Pd1—Zn3 | 83.48 (4) | Zn2 ⁱ —Zn3—Pd1 | 64.47 (4) |
| $Zn2$ — $Zn1$ — $Pd2^{v}$ | 119.582 (10) | Pd1 ^x —Zn3—Pd1 | 142.04 (5) |
| $Zn2$ — $Zn1$ — $Pd2^{iv}$ | 119.582 (10) | Pd2 ⁱ —Zn3—Zn1 | 145.42 (6) |
| $Pd2^{v}$ —Zn1—Pd2 ^{iv} | 119.582 (10) | Zn2 ⁱ —Zn3—Zn1 | 145.42 (6) |
| Zn2—Zn1—Zn2 ^v | 119.582 (10) | Pd1 ^x —Zn3—Zn1 | 61.09 (5) |
| $Pd2^{v}$ — $Zn1$ — $Zn2^{v}$ | 0.0 | Pd1—Zn3—Zn1 | 80.96 (5) |
| $Pd2^{iv}$ — $Zn1$ — $Zn2^{v}$ | 119.582 (10) | Pd2 ⁱ —Zn3—Al3 ^{xii} | 102.22 (4) |
| Zn2—Zn1—Zn2 ^{iv} | 119.582 (10) | Zn2 ⁱ —Zn3—A13 ^{xii} | 102.22 (4) |
| $Pd2^{v}$ — $Zn1$ — $Zn2^{iv}$ | 119.582 (10) | Pd1 ^x —Zn3—Al3 ^{xii} | 58.77 (4) |
| $Pd2^{iv}$ — $Zn1$ — $Zn2^{iv}$ | 0.0 | Pd1—Zn3—Al3 ^{xii} | 139.15 (3) |
| Zn2 ^v —Zn1—Zn2 ^{iv} | 119.582 (10) | Zn1—Zn3—Al3 ^{xii} | 104.13 (5) |
| Zn2—Zn1—Al3 ^v | 65.28 (2) | Pd2 ⁱ —Zn3—A13 ^{vii} | 102.22 (4) |
| $Pd2^{v}$ —Zn1—Al3 ^v | 65.28 (2) | Zn2 ⁱ —Zn3—Al3 ^{vii} | 102.22 (4) |
| $Pd2^{iv}$ —Zn1—Al3 ^v | 135.08 (8) | Pd1 ^x —Zn3—Al3 ^{vii} | 58.77 (4) |
| $Zn2^{v}$ — $Zn1$ — $Al3^{v}$ | 65.28 (2) | Pd1—Zn3—Al3 ^{vii} | 139.15 (3) |
| | | | |

supplementary materials

| $7n2^{iv}$ $7n1$ 413^{v} | 135.08 (8) | $7n1$ — $7n3$ — 413^{vii} | 104.13 (5) |
|---|-------------------------|---|------------------------|
| $Zn2$ — $Zn1$ — $Al3^{iv}$ | 135.08 (8) | $A13^{xii}$ $Zn3$ $A13^{vii}$ | 79.83 (8) |
| $Pd2^{v} - Zn1 - A13^{iv}$ | 65.28 (2) | $Pd2^{i}$ $Zn3$ $Zn3^{xii}$ | 102.22 (4) |
| $Pd2^{iv}$ $Zn1$ $Al3^{iv}$ | 65.28 (2) | $Zn2^{i}$ $Zn3$ $Zn3^{xii}$ | 102.22 (4) |
| $7n2^{v}$ $7n1$ 413^{iv} | 65.28 (2) | $Pd1^{x} - 7n3 - 7n3^{xii}$ | 58.77 (4) |
| $Zn2^{iv}$ $Zn1$ $Al3^{iv}$ | 65.28 (2) | $Pd1 - 7n3 - 7n3^{xii}$ | 139.15 (3) |
| $\Delta 13^{v} - 7n1 - \Delta 13^{iv}$ | 81 33 (6) | 7n1 $7n3$ $7n3$ $7n3$ | 104 13 (5) |
| $7n2 - 7n1 - 7n3^{V}$ | 65 28 (2) | $A13^{XII} 7n3 7n3^{XII}$ | 0.00(6) |
| $Pd2^{V} - 7n1 - 7n3^{V}$ | 65 28 (2) | $A13^{VII} Zn3 Zn3^{XII}$ | 79.83 (8) |
| $\mathbf{P}d2^{iV}$ $\mathbf{Z}\mathbf{n}1$ $\mathbf{Z}\mathbf{n}3^{V}$ | 135.08 (8) | $\mathbf{P}_{12}^{1} = \mathbf{Z}_{13}^{13} = \mathbf{Z}_{13}^{133}$ | 102 22 (4) |
| $Tu2 - \Sigma H - \Sigma H - \Sigma H S$ $Zn2^{V} - Zn1 - Zn2^{V}$ | 65 28 (2) | $7n2^{i}$ $7n2$ $7n2^{Vii}$ | 102.22(1) 102.22(4) |
| $Zn2^{iV}$ $Zn1$ $Zn2^{V}$ | 135.08 (8) | $\sum_{i=1}^{N} \sum_{j=1}^{N} \sum_{i=1}^{N} \sum_{i$ | 58 77 (4) |
| $\sum_{i=1}^{N} \sum_{j=1}^{N} \sum_{i=1}^{N} \sum_{i=1}^{N} \sum_{i=1}^{N} \sum_{j=1}^{N} \sum_{i$ | 0.00(6) | Pd1 = -Zn3 - Zn3 | 139 15 (3) |
| $A15 \longrightarrow Zn1 \longrightarrow Zn2^{V}$ | 81 33 (6) | $\frac{7}{2} \frac{7}{2} \frac{7}{2} \frac{7}{2} \frac{2}{2} \frac{2}{10} \frac{2}{10} \frac{1}{10}$ | 104.13(5) |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | 135.08 (8) | $\sum_{i=1}^{N} \sum_{j=1}^{N} \sum_{i=1}^{N} \sum_{i=1}^{N} \sum_{i=1}^{N} \sum_{i=1}^{N} \sum_{i=1}^{N} \sum_{i=1}^{N} \sum_{i$ | 70.83 (8) |
| $\Sigma n2 - \Sigma n1 - \Sigma n3$ | 155.08 (8) 65.28 (2) | A13 - Zn3 - Zn3 | (3) |
| Pd2 = Zn1 = Zn3 | 65.28 (2) | $\begin{array}{cccc} Al5 &Zn5 \\ \hline & Zn2 \\ \hline $ | 70.83 (8) |
| Pd2 = Zn1 = Zn3 | 65.28 (2) | | 79.85 (8) |
| Zn2 - Zn1 - Zn3 | 65.28 (2) | Pd2 = Zn3 = Al3 | 65.41 (4) |
| Zn2····Zn1—Zn3··· | 03.28 (2) | $Zn2^{$ | 03.41 (4) |
| $A13^{v}$ —Zn1—Zn3 ^{1v} | 81.33 (6) | $Pd1^{-}Zn3-Al3^{-}$ | 122.72 (4) |
| $A13^{1v}$ — $Zn1$ — $Zn3^{1v}$ | 0.00 (6) | Pd1—Zn3—Al3 ¹ | 58.70 (3) |
| $Zn3^{v}$ — $Zn1$ — $Zn3^{1v}$ | 81.33 (6) | $Zn1$ — $Zn3$ — $Al3^1$ | 97.39 (5) |
| Zn2—Zn1—Zn3 | 65.28 (2) | $Al3^{XII}$ Zn3 $-Al3^{I}$ | 80.50 (3) |
| Pd2 ^v —Zn1—Zn3 | 135.08 (8) | Al3 ^{vii} —Zn3—Al3 ⁱ | 153.76 (7) |
| $Pd2^{iv}$ —Zn1—Zn3 | 65.28 (2) | $Zn3^{xii}$ — $Zn3$ — $Al3^{i}$ | 80.50 (3) |
| $Zn2^{v}$ — $Zn1$ — $Zn3$ | 135.08 (8) | Zn3 ^{vii} —Zn3—Al3 ⁱ | 153.76 (7) |
| Zn2 ^{iv} —Zn1—Zn3 | 65.28 (2) | Pd2 ⁱ —Zn3—Al3 ⁱⁱ | 65.41 (4) |
| Al3 ^v —Zn1—Zn3 | 81.33 (6) | Zn2 ⁱ —Zn3—Al3 ⁱⁱ | 65.41 (4) |
| Al3 ^{iv} —Zn1—Zn3 | 81.33 (6) | Pd1 ^x —Zn3—Al3 ⁱⁱ | 122.72 (4) |
| Zn3 ^v —Zn1—Zn3 | 81.33 (6) | Pd1—Zn3—Al3 ⁱⁱ | 58.70 (3) |
| Zn3 ^{iv} —Zn1—Zn3 | 81.33 (6) | Zn1—Zn3—Al3 ⁱⁱ | 97.39 (5) |
| Pd2 ^{vi} —Zn2—Zn2 ^{vi} | 0.0 | Al3 ^{xii} —Zn3—Al3 ⁱⁱ | 153.76 (7) |
| Pd2 ^{vi} —Zn2—Al3 ^{vii} | 68.97 (4) | Al3 ^{vii} —Zn3—Al3 ⁱⁱ | 80.50 (3) |
| Zn2 ^{vi} —Zn2—A13 ^{vii} | 68.97 (4) | Zn3 ^{xii} —Zn3—Al3 ⁱⁱ | 153.76 (7) |
| Pd2 ^{vi} —Zn2—Zn3 ^{vii} | 68.97 (4) | Zn3 ^{vii} —Zn3—Al3 ⁱⁱ | 80.50 (3) |
| Zn2 ^{vi} —Zn2—Zn3 ^{vii} | 68.97 (4) | Al3 ⁱ —Zn3—Al3 ⁱⁱ | 111.69 (7) |

Symmetry codes: (i) -y+1/2, z+1/2, -x+1/2; (ii) z+1/2, -x+1/2, -y+1/2; (iii) -x+1/2, -y+1/2; z+1/2; (iv) z, x, y; (v) y, z, x; (vi) -x+1, -y, z; (vii) -z+1/2, -x+1/2, y-1/2; (viii) -z+1/2, x-1/2, -y+1/2; (ix) x, -y, -z; (x) -x+1/2, -y+1/2, z-1/2; (xi) -x+1/2, y-1/2, -z+1/2; (xii) -y+1/2, -z+1/2, x-1/2.



Fig. 1

